

REPORT# 10543-xiv/GSK

GEOTECHNICAL INVESTIGATION REPORT

Location	Mia Noor, Fateh Jang
Project	Government Boys Primary School.
No. of Bore Holes	02
Date of Exploration	August, 2023
Reporting Officer	Engr. Ghassan Sattar Khan
Submitted to:	UNHCR
Ground Water Table Depth	02ft
Recommended net bearing capacity	0.50 TSF







Contents Table 1.00 – INTRODUCTION	2
Table 1.10 – GENERAL	2
Table 1.20 – ACTIVITY DETAILS	3
Table 2.00 – EVALUATION	3
Table 3.00 - CONCLUSION	4
3.10 Bearing Capacity (In-situ Condition)	4
3.20 Site Class	4
3.30 Seismic Zone	4
Table 4.00 - RECOMMENDATION	5
4.10 Backfill Material	5
4.20 Site Drainage	5
SITE PICTURES	6
A.1.0 PURPOSE OF GEOTECHNICAL INVESTIGATION	8
A.2.0 METHODOLOGY	8
A.2.1 Field Work	8
A.2.2 Laboratory Work	9
A.2.2.1 Moisture Content & Bulk Density	9
A.2.2.2 Partical Size Distribution	10
A.2.2.3 Atterberg's Limits	10
A.2.2.4 Unconfined Compression Test:	11
B.1.0 BEARING CAPACITY CALCULATION:	12
B.1.1 Bearing Capacity from c &.	12



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Table 1.00 – INTRODUCTION									
Table 1.10 – GENERAL									
Client Name	UNHCR								
Hiring of services By	UNHCR								
Location/ Address	Mia Noor Fateh Jang								
Borehole Layout Plan & Site Location Government Boys Government Boys Cont High School Temporarive centre Government Boys Cont Girls Cont High School									
Name of Project	Construction of Government Boys Primary School.								
No. of Stories	Single story								
Task To be Performed	Geotechnical Investigation								
Scope of Work/ Work executed	02 Bore Hole. (up to 15ft depth)								
Purpose of activity	Geotechnical Investigation								
Arial Conditions of the site Plot level was at road level.									





Table 1.20 – ACTIVITY DETAILS								
Coordinates of exploratory points		(33.64	8518919064614, 72.617364082230)3)				
Field Tests performed		i. II.	Drilling of Bore Holes Conduction of SPT	02 Each at 05ft interval				
Observed telephone lines, sewer lin poles, water pipes etc.	nes, electric	None						
Laboratory Tests performed		i. ii. iii. iv.	Atterberg's limits <i>ASTM D-4318-10.</i> Particle Size <i>ASTM D422, D1140.</i> Unconfined Compression tests <i>ASTM D-2166</i> Direct shear tests <i>ASTM D-3060</i>	02 02 02 01				
Ground Water Table from N.S.L	2ft	Ground	d Water Table from R.L	2ft				
Encountered Rocky Strata depth	Nil	Seepa	ges	Not recorded				

Table 2.00 – EVALUATION											
S. No.	Depth (ft.)										
01	0-5 The strata encountered up to depth 5ft was Lean Clay. Percentage of fines ranged 86.9% to 87.2% and percentage of sand was found to be 12.7% to 13%.										
02	6 - 15	According to USCS classification the strata mainly comprised of si fines ranged 88% to 89.1%. percentage of Sand ranged 10% to 1	, , ,								
02 Tests performed to measure the shear strength parameters of soil according to the ASTM, to analyze the bearing capacity of the strata. Unconfined 02 Shear tests											





	Table 3.00 - CONCLUSION										
3.10 Be	3.10 Bearing Capacity (In-situ Condition)										
S. No Depth (ft.) Footing Vidth Capacity (ft.) Type Width (ft.) TSF TSF TSF TSF TSF TSF											
01	04	Strip	05	2.10	0.70	0.50					
3.20 Sit	e Class				·	·					

Average Properties for Top 30 M (100 ft) of Soil Profile Soil Profile Soil Profile Name/ Shear Wave Velocity, Standard Penetration Tests, Undrained Shear Strength, s_s Туре Generic Description N [or N_{CH} for cohesionless kPa v, m/sec (ft/sec) soil layers] (blows/foot) (psf) >1.500 S_A Hard Rock (>4,920) 750 to 1,500 Rock (2,460 to 4,920) S_B 350 to 750 >100 Very Dense Soil and S_C (1,150 to 2,460) >50 (>2,088) Soft Rock 50 to 100 175 to 350 Stiff Soil Profile (575 to 1,150) 15 to 50 (1,044 to 2,088) S_D <50 <175 S_E^{-1} <15 Soft Soil Profile (<1,044) (<575) Soil requiring Site-specific Evaluation. See 4.4.2 S_F

1 Soil Profile Type S_E also includes any soil profile with more than 3 m (10 ft) of soft clay defined as a soil with a plasticity index, PI > 20, $w_{mc} \ge 40$ percent and $s_u \le 25$ kPa (522 psf). The Plasticity Index, PI, and the moisture content, w_{mc} , shall be determined in accordance with the latest ASTM procedures.

Site Class	From 04ft $-$ 08ft S _E ¹
Ref: Pakistan Building Code 2007	
3.30 Seismic Zone	Zone : 2B PGA of 0.16g to 0.24g.
Ref: Pakistan Building Code 2007	





Table 4.00 - RECOMMENDATION

- i. Compact the surface prior to laying foundation.
- ii. It is recommended to provide pure gravel layer of thickness not less than 18inches below footing compacted properly in layers.

4.10 Backfill Material

In general, materials for the backfilling should be granular, not containing rocks or lumps over 15 cm in greatest dimension, free from organic matter, with plasticity index (PI) not more than 6%. The backfill material should be laid in lifts not exceeding 25 cm in loose thickness and compacted to at least 95 percent of the maximum dry density at optimum moisture content as determined by modified compaction test (Proctor) (ASTM D-1557).

4.20 Site Drainage

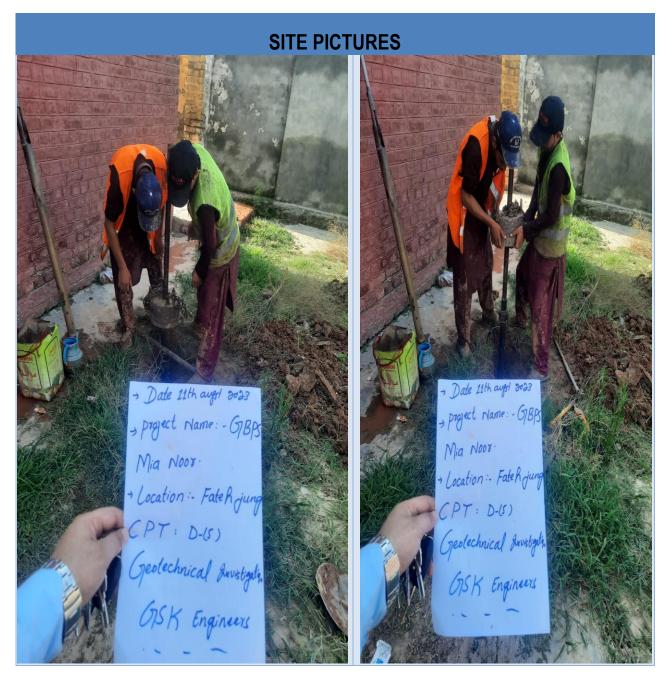
It is recommended to design an effective rainwater drainage system to get rid of the consequences of the rainwater percolation into the layers *(i.e. provision of parametric drains)*. The site should be graded so as to direct rainwater and water away from all planned structures. Under no circumstances, the foundation shall get inundated during the whole period of construction. Utmost care shall be taken not to allow drainage water to seep into the soil.

For this specific water logged site, simultaneous dewatering activity must be carried out along with excavation. This may be done using test pits or filter piles / boreholes.

Reporting Officer









Address: 97-K Industrial Estate, Hayatabad Peshawar Phone: 091-5881841, Cell No: 0333-5177774 e-mail.pce.pesh@gmail.com



ANNEXURE-A SCOPE OF WORK & METHODOLOGY



Address: 97-K Industrial Estate, Hayatabad Peshawar Phone: 091-5881841, Cell No: 0333-5177774 e-mail.pce.pesh@gmail.com



A.1.0 PURPOSE OF GEOTECHNICAL INVESTIGATION

The very main purpose of Geotechnical investigation is to conduct soil investigation for the site where building construction needs to take place.

The activity comprises of soil exploration and determines suitability of the site for the proposed construction. It mainly helps in knowing which type of foundation is required or what safety measures shall be taken. The effort and detail of geotechnical site investigation is to obtain sufficient and correct site information so as to select and design a foundation for a building that is most economical and appropriate.

In general, the purpose of this site investigation was to provide the following:

1- Information to determine the type of foundation required (shallow or deep).

2- Information to allow the geotechnical consultant to make a recommendation on the allowable bearing capacity of the soil.

- 3- Sufficient data/ laboratory tests to make settlement and swelling predictions.
- **4-** Location of the groundwater level
- 5- Information so that the identification and solution of excavation problems can be made.

A.2.0 METHODOLOGY

A.2.1 Field Work

a. Preliminary survey

Preliminary survey was conducted by the team to identify drilling points location based on master plan for the building.







b. Drilling

As per scope of work, the site investigation program included the exploration of site subsurface conditions through the drilling of **two boreholes**, up to 15ft deep below the existing ground level.

c. Sampling

Samples collected:

 \checkmark <u>Disturbed samples;</u> for identification and index property testing purposes at various depths as elucidated in the scope of work.

✓ <u>Undisturbed samples;</u> for the computation of shear strength parameters of soil. The samples were collected using Block Sampling method.

Representative samples were placed in sealed plastic bags and core boxes, to be transported to the laboratory for further testing.

A.2.2 Laboratory Work

A.2.2.1 Moisture Content & Bulk Density

To determine the moisture content of soils, the soil sample was dried at a temperature of 105°C to 110°C for about 24 hours. The loss in weight of the soil sample represented the weight of moisture in the soil. The moisture content of the soil to the dry weight of soil in percentage is the moisture content of the testing soil. This test was performed in accordance with BS 1377: Part 2: 1990. The bulk density of a soil, i.e. the mass per unit volume of the soil deposit including any water it contains was determined at the laboratory by using the linear measurement method approached by BS 1377: Part 2: 1990.





A.2.2.2 Partical Size Distribution

Particle size distribution was determined by means of sieving. Sieves of standard sizes were used as per ASTM E11-09e1. The percentage of weight of the various particle sizes were determined by sieving through a set of these standard sieves. This test was performed to determine the percentage of different grain sizes contained within a soil sample. This test was performed as per ASTM D422, D1140. Graphs obtained are attached in the appendices.



A.2.2.3 Atterberg's Limits

Following ASTM D4318-10, the liquid limit and plastic limit of required sample that is cohesive in nature, was computed. The Atterberg's limits refer to arbitrarily defined boundaries between the liquid and plastic states (i.e., liquid limit, W_L) and between the plastic and brittle states (ie, plastic limit, W_P), of



fine grained soils. They are expressed in percentage water content. The range of water contents over which a soil behaves plastically is termed the Plastic Index and corresponds to the numerical difference between the liquid and plastic limit (ie, W_rW_P).

The liquid limit (LL) is arbitrarily known as the water content, in percent, at which a pat of soil in a standard cup and cut by a groove of standard dimensions will flow together at the base of the groove for a distance of 13 mm (1/2 in.) when subjected to 25 shocks from the cup being dropped 10 mm in a standard liquid limit apparatus operated at a rate of two shocks per second. The typical cassagrande's apparatus was used in determination of Liquid Limit.

The plastic limit (PL) is the water content, in percent, at which a soil can no longer be deformed by rolling into 3.2 mm (1/8 in.) diameter threads without crumbling





A.2.2.4 Unconfined Compression Test:

The test was conducted as per ASTM-D2166. In this test Method, a cylindrical soil specimen is unconfined laterally while loaded axially at an axial strain rate between 0.5 to 2 %/min. Measurements are made of elapsed time, axial deformation, and axial load. The unconfined compressive stress, qu, is calculated as the compressive stress at failure. The undrained cohesion, cu, is one half of the unconfined compressive strength. The primary purpose of the unconfined Compressive is to quickly obtain a measure of compressive



strength for those soils that possess sufficient cohesion to permit testing in the unconfined state.





B.1.0 BEARING CAPACITY CALCULATION:

The bearing capacity of soil is the average contact <u>stress</u> between a <u>foundation</u> and the soil which will cause shear failure in the soil. Allowable bearing stress is the bearing capacity divided by a factor of safety.

Following method was adopted to compute the bearing capacity values;

- i. From c &φ
- ii. From SPT (In-Situ Testing)

B.1.1 Bearing Capacity from c $\& \phi$

Terzaghi's equation has been used to calculate the bearing capacity for cohesive soils. A factor of safety of '03' is used in calculation of Allowable bearing capacity. Data received from direct shear test has been used in the following equation.

Qu =1.3
$$cNc$$
+ $qNqRw_1$ +0.4 $\gamma BN\gamma Rw_2$

C = Cohesion of soil, γ = unit weight of soil, D = depth of footing, B= width of footing

C,Ø - Strength parameters of the soil below foundation level.L - Length of foundation.

Nc, Nq, Ny - Bearing capacity coefficients dependent on the angle of internal friction of the soil.

Nc = cot ϕ (Nq -1), N_q = $e^{\pi tan\phi_tan^2(45+\phi/2)}$] N_γ = (Nq - 1) tan(1.4 ϕ) ,Kp = tan²(45 + $\phi/2$)





	Mayerhoff's Bearing Capacity Factors								
Ø	Nc	Nq	Ny						
0	5.1	1	0						
5	6.5	1.6	0.1						
10	8.3	2.5	0.4						
15	11	3.9	1.2						
20	14.9	6.4	2.9						
25	20.7	10.7	6.8						
30	30.1	18.4	15.1						
35	46.4	33.5	34.4						
40	75.3	64.1	79.4						





	Table 1.1: Summary of Soil Classification, Strength and Parameter											
No.	Location	Depth (ft)	Gravel (%)	Sand (%)	Fines (%)	Fineness Modulus	Liquid Limit (%)	Plastic Limit (%)	Plastic Limit (%)	Classification (USCS)		
1	ole#1	10	0.1	13.0	86.9	0.32	23.8	10.0	13.8	CL, Lean Clay		
2	Bore hole#1	10 - 15	0.0	11.8	88.2	0.29	23.8	19.4	4.4	CL - ML, Silty Clay.		
3	ole # 2	10	0.1	12.7	87.2	0.32	20.6	7.9	12.8	CL, Lean Clay		
4	Bore hole	10 - 15	0.0	10.9	89.1	0.27	23.7	19.5	4.2	CL - ML, Silty Clay		

Flat No. 205 & 206, Afzal Tower, Behind Shahab Ortho-Hospital, Phase III Chowk, Peshawar. Email: <u>gsk.engineerz@gmail.com</u>, 0333-912-6118, 091-584-1515



BOREHOLE LOG & STANDARD PENETRATION TESTING (ASTM-1586-54)										
BH No.: 1 Drilling Method : Light Percussion										
Date of			Aug,	2023		Report No.	10543-xiv/GSK			
	•									
Assum	ed footir	ng width	(ft)=	6		Name of Project:	Construction of Governmer	t Boys Primary School		
Boreho	le diame	eter (Inch	nes)=	3		Client:	UNHCR			
			C _{S=}	1		Location:	Fateh Jang			
			C _{B =}	1		Depth of Borehole	15ft			
			E _{m=}	0.55		Water Table Depth	2ft			
Select I	Efficienc	y Correc	ction	N70		Name of Tech:	Zohaib Ahmed			
Depth	Penetration		on	N- Value	N70	N70 Vs Depth	Soil Classification	Soil Profile		
ft	6-in	6-in	6-in	ii vulue						
5	6	6	5	11	6.5	0.0 5.0 10.0	Lean Clay			
10	4	4	5	9	5.3	10	CL-ML, Silty Clay			
15	5	5	4	9	6.0	15	CL-ML, Silty Clay			

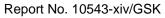




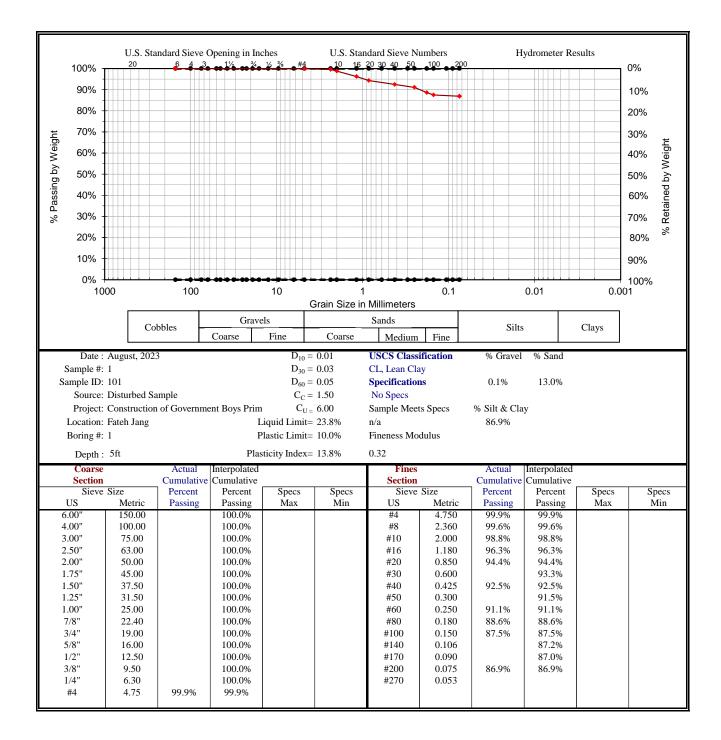
BOREHOLE LOG & STANDARD PENETRATION TESTING (ASTM-1586-54)										
BH No.: 2			Drilling Method :	Light Percussion						
Date of	Driling:		Aug, 2	2023		Report No.	10543-xiv/GSK			
Assum	ed footir	ng width	(ft)=	6		Name of Project:	Construction of Government Boys Primary School			
Boreho	le diame	ter (Inch	nes)=	3		Client:	UNHCR			
			C _{S=}	1		Location:	Fateh Jang			
			C _{B=}	1		Depth of Borehole	15ft			
			E _{m=}	0.55		Water Table Depth	2ft			
Select I	Efficienc	y Correc	ction	N70		Name of Tech:	Zohaib Ahmed			
Depth	Pe	enetratio	on	N- Value	N70	N70 Vs Depth	Soil Classification	Soil Profile		
ft	6-in	6-in	6-in							
5	5	5	6	11	6.5	6.4 6.6 6.8	Lean Clay			
10	4	5	6	11	6.5	10	CL-ML, Silty Clay			
15	4	5	5	10	6.7	15	CL-ML, Silty Clay			







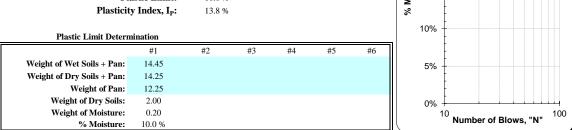


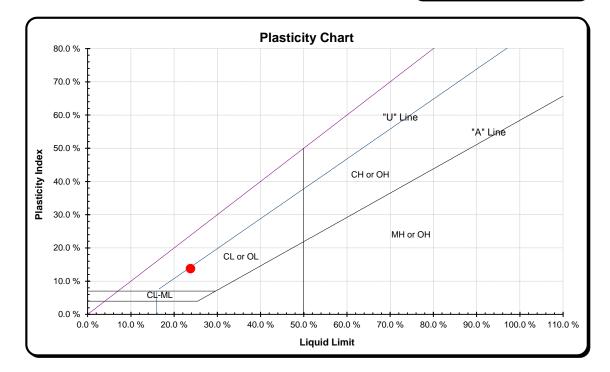




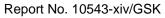


Date Received: August, 2023 Project: Construction of Government Boys Primary School Sample #: 1.00 Location: Fateh Jang Sample ID: 101.00 Boring #: 1 Depth: 5ft Source: Disturbed Sample ASTM D-2487, Unified Soils Classification System CL, Lean Clay Liquid Limit Determination #2 #3 #4 #5 #6 #1 **Liquid Limit** Weight of Wet Soils + Pan: 53.99 46.99 33.56 30% Weight of Dry Soils + Pan: 46.23 41.02 30.85 Weight of Pan: 16.55 17.88 16.99 Weight of Dry Soils: 29.24 24.47 12.97 25% Weight of Moisture: 7.76 5.97 2.71 % Moisture: 26.5 % 24.4 % 20.9 % 13 25 35 N: 20% % Moisture Liquid Limit @ 25 Blows: 23.8 % 15% **Plastic Limit:** 10.0 %

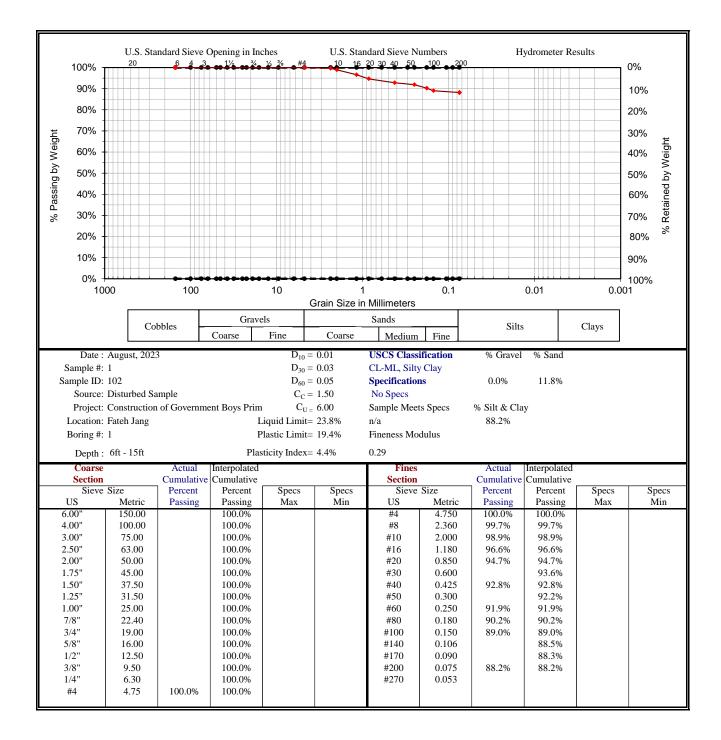


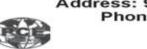














Weight of Wet Soils + Pan:

Weight of Dry Soils + Pan:

Weight of Pan:

% Moisture:

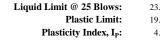
Weight of Dry Soils:

Weight of Moisture:

PLANNERS CONSULTANTS ENGINEERS

#6

Date Received: August, 2023 Project: Construction of Government Boys Primary School Sample #: 1.00 Location: Fateh Jang Sample ID: 102.00 Boring #: 1 Depth: 6ft - 15ft Source: Disturbed Sample ASTM D-2487, Unified Soils Classification System CL-ML, Silty Clay Liquid Limit Determination #2 #3 #4 #5 #6 #1 **Liquid Limit** Weight of Wet Soils + Pan: 53.99 46.99 33.56 30% Weight of Dry Soils + Pan: 46.23 41.02 30.85 Weight of Pan: 16.55 17.88 16.99 Weight of Dry Soils: 29.24 24.47 12.97 25% Weight of Moisture: 7.76 5.97 2.71 % Moisture: 26.5 % 24.4 % 20.9 % 13 25 35 N: 20%



14.45

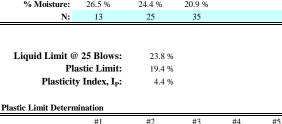
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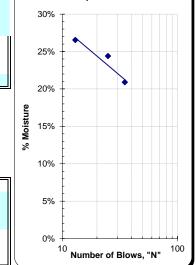
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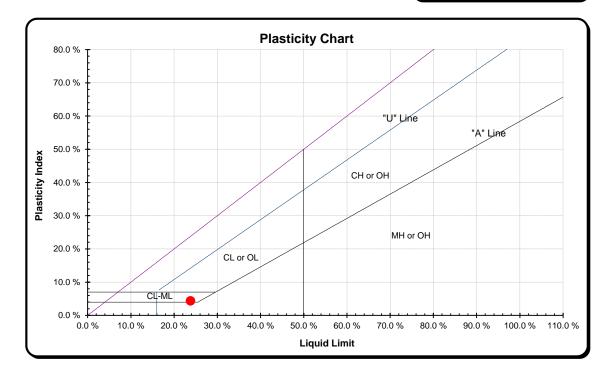
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0.20

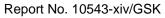
19.4 %



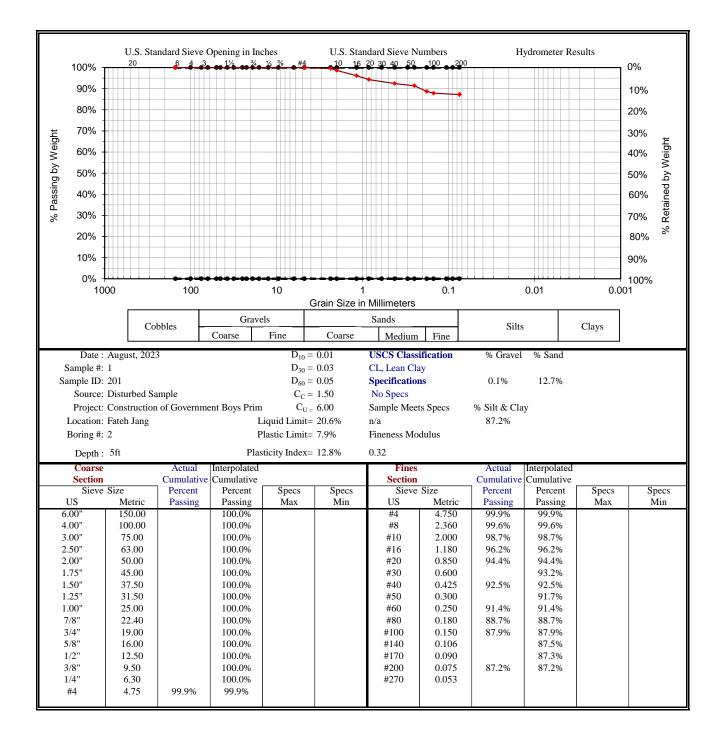
















Weight of Wet Soils + Pan:

Weight of Dry Soils + Pan:

Weight of Pan:

% Moisture:

Weight of Dry Soils:

Weight of Moisture:

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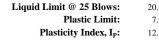
Date Received: August, 2023 Project: Construction of Government Boys Primary School Sample #: 1.00 Location: Fateh Jang Sample ID: 201.00 Boring #: 2 Depth: 5ft Source: Disturbed Sample ASTM D-2487, Unified Soils Classification System CL, Lean Clay Liquid Limit Determination #2 #3 #4 #5 #6 #1 **Liquid Limit** Weight of Wet Soils + Pan: 54.12 45.23 33.01 30% Weight of Dry Soils + Pan: 46.53 39.98 30.95 Weight of Pan: 14.22 17.99 17.99 Weight of Dry Soils: 28.54 25.7612.96 25% Weight of Moisture: 7.59 5.25 2.06 % Moisture: 26.6 % 20.4 % 15.9 % 25 35 N: 13 20%

#4

#5

#6

#3



#1

14.42

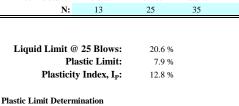
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12.23

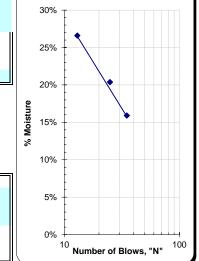
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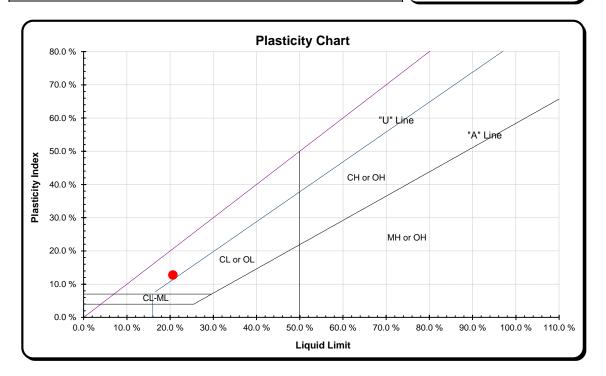
0.16

7.9 %



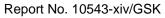
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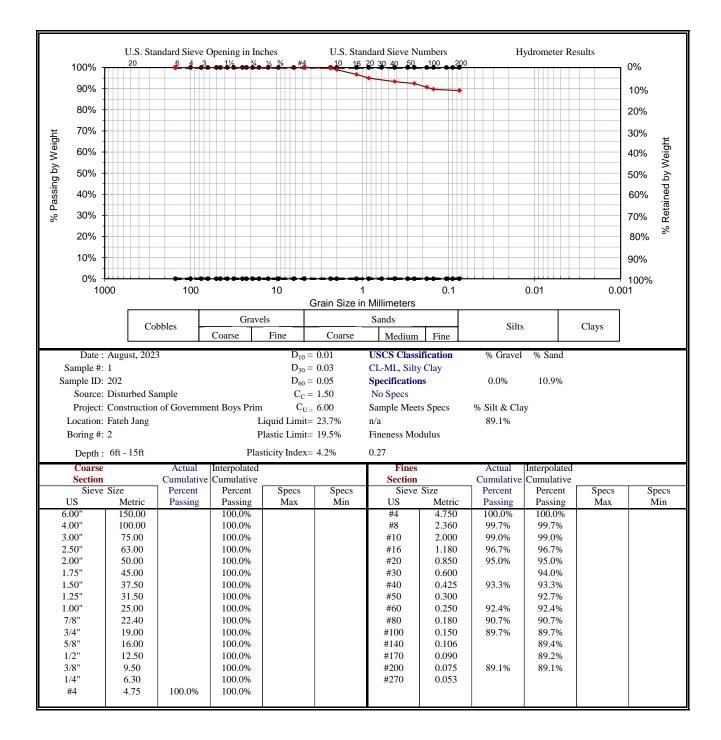


















Date Received: August, 2023 Project: Construction of Government Boys Primary School Sample #: 1.00 Location: Fateh Jang Sample ID: 202.00 Boring #: 2 Source: Disturbed Sample Depth: 6ft - 15ft ASTM D-2487, Unified Soils Classification System CL-ML, Silty Clay Liquid Limit Determination #2 #3 #4 #5 #6 #1 **Liquid Limit** Weight of Wet Soils + Pan: 54.02 47.02 33.58 30% Weight of Dry Soils + Pan: 46.22 41.01 30.95 Weight of Pan: 17.06 16.48 18.02 Weight of Dry Soils: 29.16 24.53 12.93 25% Weight of Moisture: 6.01 7.80 2.63 % Moisture: 26.8 % 24.5 % 20.3 % 13 25 N: 35 20% % Moisture Liquid Limit @ 25 Blows: 23.7 % 15% Plastic Limit: 19.5 % Plasticity Index, I_P: 4.2 % 10%

Plastic Limit Determ	-							
	#1	#2	#3	#4	#5	#6	-	
Weight of Wet Soils + Pan:	14.46						5%	
Weight of Dry Soils + Pan:	14.24							
Weight of Pan:	13.11						-	
Weight of Dry Soils:	1.13						0%	
Weight of Moisture:	0.22						10	100
% Moisture:	19.5 %							Number of Blows, "N"

